

Assessing Aquifer Capacity for SAGD Development

Luis E. Rivera, P. Geol., Michael J. Doty, P. Geoph. Sunshine Oilsands Ltd, Calgary

Key Words: SAGD, aquifer, capacity, well efficiency, prolific

Summary

It has become of high interest in steam assisted gravity drainage (SAGD) to know how much water is an aquifer capable of producing and how dependable its production will be with time. Aquifer capacity is determined by Transmissivity (T) as derived from pumping tests. Although the aquifer testing theory provides analytical solutions to estimate T, data collected for interpretation may be negatively impacted by well efficiency, a quality-indicator of well completion. Thus, a close approximation of aquifer capacity – a reliable T – can only be derived by testing highly efficient wells. This assessment was initiated to investigate aquifer capability of delivering water for SAGD schemes. The results show that average geometric mean Transmissivity was 103 m²/day, which is an indication of a prolific aquifer. Average Q_{20} rate was 619 m³/day.

Introduction

Water production in a well is a function of aquifer capacity and well efficiency. Capacity is conventionally determined by Transmissivity (T). The higher the Transmissivity, the more prolific the aquifer, with less potential for depletion. While T is set by the bulk of aquifer properties and the hydrodynamic regime, well efficiency varies depending on individual well installations. Low efficiency resulting from poorly installed wells may negatively impact water production, lowering it below natural yield. Thus, a close approximation of aquifer capacity – a reliable T – can only be derived by testing highly efficient wells

Theory and Methods

Well efficiency is defined as the ratio of the theoretical drawdown in the aquifer to the actual drawdown in the well. The difference between the two is caused by head losses of the water as it moves from the formation to the surface. Well efficiency is calculated from step rate tests (SRT) data. The *Hantush* (1964), *Bierschenk* (1964) and *Todd* (1980) methods were used to estimate well efficiency.

GeoConvention 2014: FOCUS

$$Efficency = {}^{BQ}/S_{W_{THEOR}}$$
 (3), Todd (1980)

Where B represents the linear well loses coefficient, Q is the pumping rate and S_{wTHEO} is the theoretical drawdown. Specific capacity is calculated as SC = 1/B. Transmissivity from SRT data is calculated as $T\sim1.4SC$ and is compared to values derived from constant rate tests (CRT) data. This comparison is useful to later assess heterogeneity.

A total of six water source wells (WSW) were installed and tested for the purpose of this assessment. Each WSW was installed using the telescopic screen method and coupled with an observation well. Aquifer testing consisted of SRT, each one with three to six pumping steps, 30 to 45 minutes long. Step rate tests were followed by long-term, 72-hour CRT.

Examples

Summary results from aquifer testing conducted on each WSW, including the sustainable rate Q₂₀ assessment using the *Moell Method* (GoA 2011) are presented in Table 1. Testing results did not indicate presence of boundary conditions (recharge or impermeable barriers).

Table 1 – Summary results from aquifer testing

Well Id	Aquifer Thickness (m)	Available Head ¹ (m)	Sustainable Rate-Q ₂₀ (m³/day)	Step Rate Test -Q (m²/day)	Constant Rate-Q (m³/day)	Constant Rate -T (m²/day)	Refined Specific Capacity ² (m³/day/m)	Well Efficiency % (Hi –Low)
PW-01	50.0	33.1	520	71.1	300	98.8	50.76	95-87
PW-02	46.0	33.3	605	64.5	850	76.9	46.08	93-88
PW-03	46.4	11.4	452	133.3	586	142.0	95.24	98-94
PW-04	62.0	20.3	1244	269.2	1500	190.0	192.31	85-80
PW-05	26.4	26.0	248	36.6	323	32.3	26.11	91-85
PW-06	61.0	24.9	1244	181.8	1000	179.1	129.87	97-91
Geome	Geometric Mean		619		611	103	73	

Above the top of the aquifer

Results of the well efficiency assessment are shown in Figure 1 and indicate that all wells were efficiently installed with efficiencies between 80% and 100%. Figure 2 shows that T values from SRT and CRT are close to a 1:1 ratio; therefore, T would closely represent the aquifer capacity at the given locations. As efficiency decreases, (e.g. well PW-04) T values are no longer close to a 1:1 ratio. Magnitude of the deviation depends directly on well efficiency – the lower the efficiency, the greater deviation. Thus, aquifer capacity in well PW-04 is expected to be higher when pumping out of more efficient wells (i.e. close to 269. m^2 /day from SRT). Figure 2 also illustrates that the aquifer is quite homogeneous. In highly efficient wells, close correlation of T values from SRT and CRT suggest no boundary conditions, barriers, or major heterogeneities, for which T values will potentially deviate from a 1:1 ratio.

GeoConvention 2014:Focus 2

²Calculated from step rate tests (SRT)

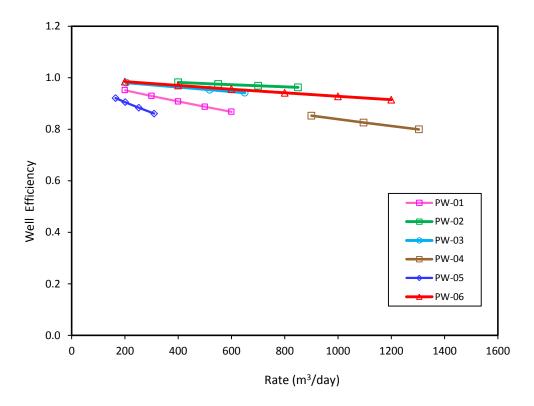


Figure 1 Well efficiency

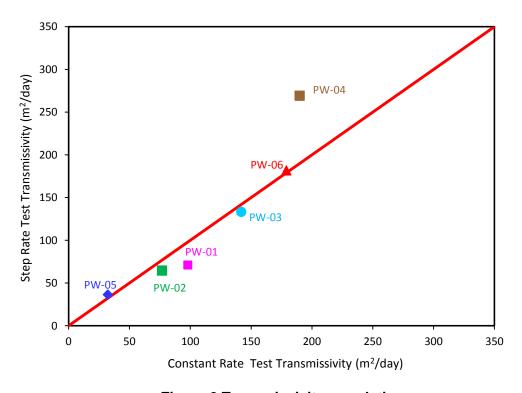


Figure 2 Transmissivity correlation

GeoConvention 2014:Focus 3

Conclusions

Results indicate that the assessed aquifer is prolific with enough capacity (7) of water supply for SAGD development. The geometric mean Transmissivity, approximately 103 m²/day, is indicative of a prolific aquifer. Geometric mean for specific capacity of 73 m³/day/m is also indicative of a prolific aquifer. The Geometric mean for Q₂₀, for single well pumping rates, is 619 m³/day.

Acknowledgements

Special thanks to Sunshine Oilsands Ltd. for facilitating the data and divulgation. Kimberly Taschuck for her comments.

References

Bierschenk W.H., 1964. Determination of Well Efficiency by Multiple Step-drawdown Tests. International Association of Scientific Hydrology. Publ 64.

Hantush .S., 1964. Hydraulic of Wells, Advances in Hydroscience, Volume1. Academic Press. New York and London Government of Alberta (GoA), 2011 Alberta Environment Guide to Groundwater Authorization

Matrix Solutions Inc., 2013. Groundwater Supply Well Testing and Evaluation. Sunshine Oilsands Ltd. West Ells Water Project 14-32-094-17 W4M

Matrix Solutions Inc., 2013. Groundwater Supply Well Testing and Evaluation. Sunshine Oilsands Ltd. West Ells Water Project 11-03-095-17 W4M AND 16-30-094-17 W4M

Todd, D.K. Groundwater Hydrology, second edition. Wiley, 1980. pp 556.

Waterline Resources Inc., 2013. Legend Lake Groundwater Supply Development Program, 01-20-096-18-W4M and 07-21-096-18-W4M west of Fort MacKay, Alberta.

Waterline Resources Inc., 2012. Regional Viking Formation Geological and Hydrogeological Mapping Study, T91-100, R12-24 W4M, Northeast Alberta

Waterline Resources Inc., 2012. West Ells Groundwater Supply Development Program 16-32-094-17-W4M & 10-33-094-17-W4M, West of Fort MacKay, Alberta

GeoConvention 2014:Focus 4